

Detector Construction & Installation

w.j. llope

☆ *TOF DOE Review, BNL*

August 22, 2005

Outline:

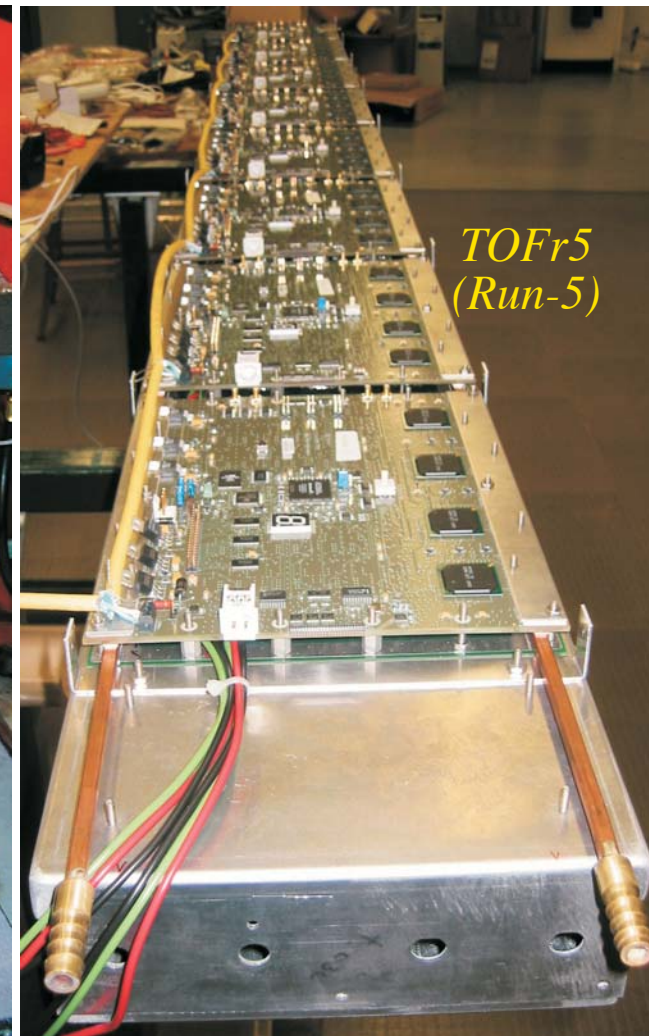
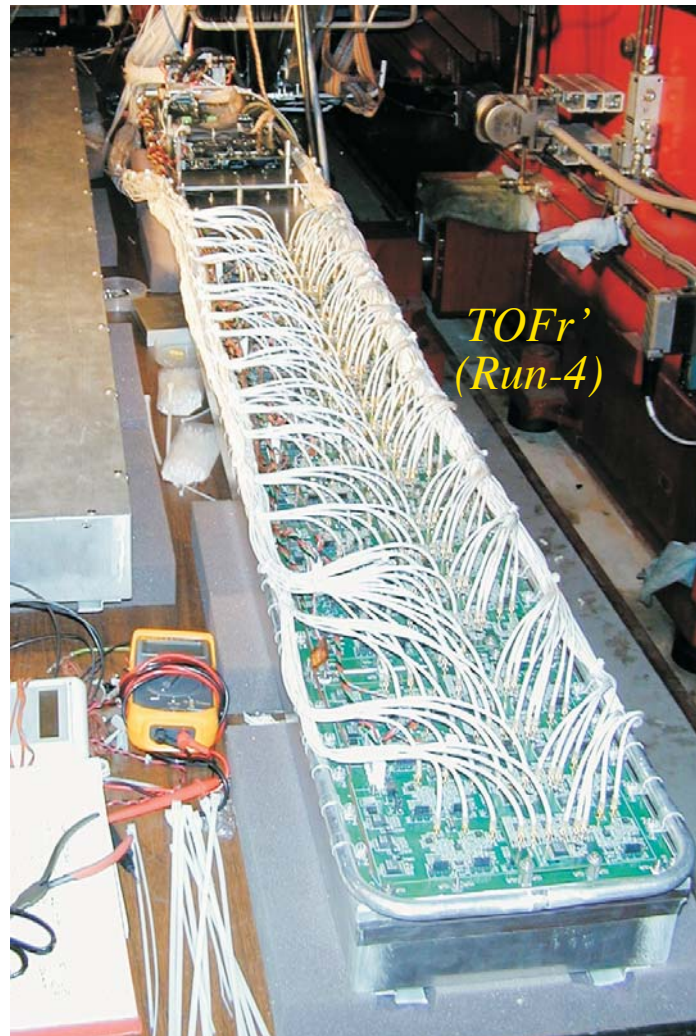
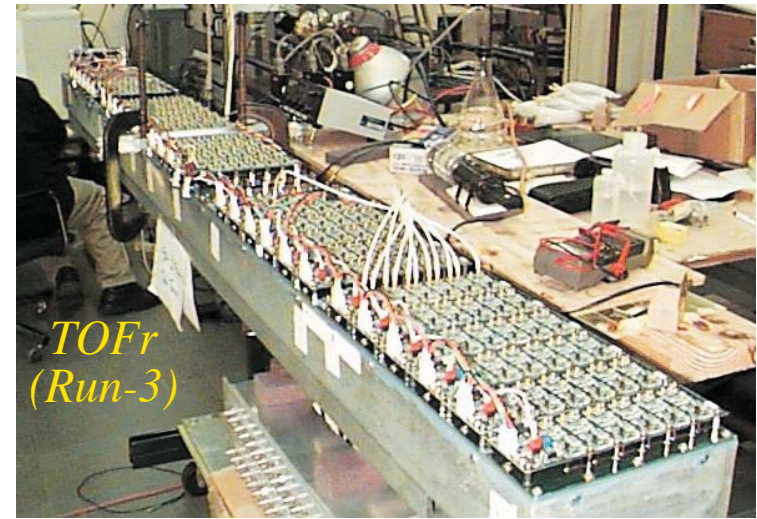
- Tray mechanical design
TOFr, TOFr', TOFr5, & TOFr6
- Impact of full system on STAR
weight
power & temperature
secondary production
gas containment
- Tray Fabrication
space and fixtures
detailed procedure
126 tray production plan
- Start detector
simulations
new based development
Run-6 prototype

Mechanical Design Summary

3 generations of TOFr trays
(all rebuilt from the ground up)
all met the physics goals

subsequent trays (TOFr6, ...) will be
simple variants of the TOFr5 design:

- simple, quick, & repeatable to assemble
- very precise detector positioning
- open-box MRPC → FEE testing



Overview of TOFr5 Design

Effects on other STAR subsystems

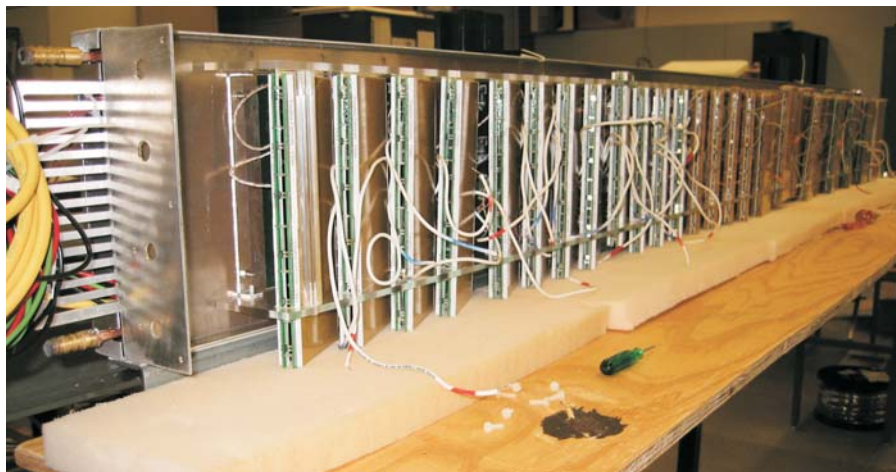
- weight
- power, cooling, & temperature
- interaction and radiation lengths
- gas containment

D&M: TOFr5 (Run-5)

First attempt at on-board digitization
Back to two layers of on-board electronics
Integrated cooling loop
new batches of MRPCs (USTC & Tsinghua)

“Inner Sides” instead of sawtooths...

lexan machined on hurco machine to few mils
MRPCs held in reveals cut into the inner sides
Inner sides bolt to underside of top assy



perf. cover assy

cooling loop

- ~~fabrication extremely labor intensive...~~
~~sawtooths, rail assy~~
- ~~complicated gas sealing...~~
~~gaskets, less sealant~~
- ~~MRPC placement w/in box too imprecise...~~
~~each sawtooth placed individually~~
- ~~overall, too tall~~

“bowing” of bottom assy due to welded feet
small tweaks to box & inner sides design
integration of TINO, TDIG version 2, & cooling

TOFr5 cooling loop tests & efficiency/power estimates:
http://wjlllope.rice.edu/~TOF/TOFr5/Ttests/TOFr5_T_tests.htm

4th Generation Prototype (TOFr6)

simpler cooling loop design

1/4" square → 1/4"x3/8" rectangular

only small tweaks to mechanical design

TINO

new cooling loop

tweaks to tray fabrication

bowing from welded feet

(moving back to pop-rivets)

TINO

lower power

no ringing

fully differential

multiplicity outputs

now only need positive LV!

TDIGb

accepts signals from TINO

(remove discriminators)

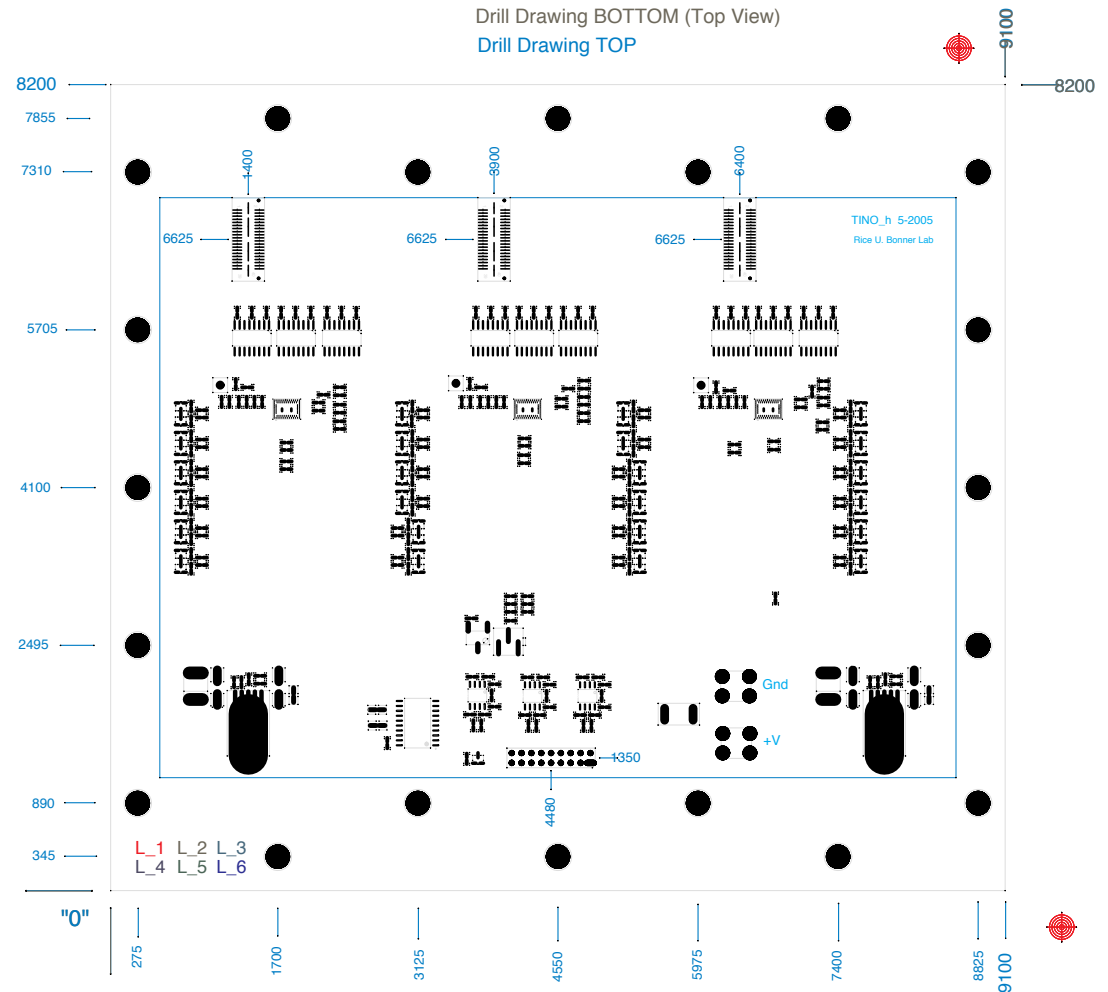
address timing cross-talk

multiplicity

Tentative Stop-side detectors for Run-6

2 trays with single-stack modules

with "TOFr6" mechanical design



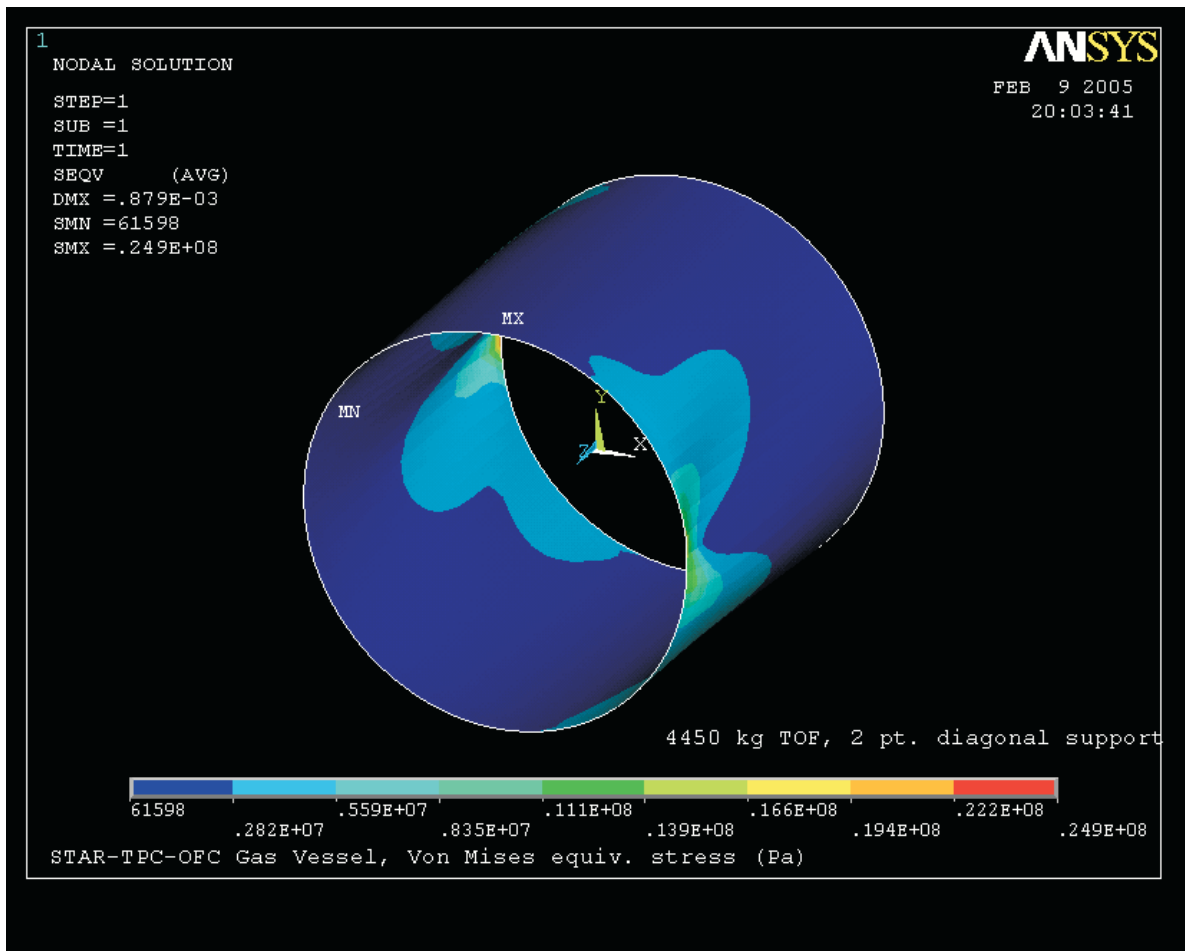
Weight issues

each TOF tray is ~75 lbs, 9,000 lbs total
what are the mechanical safety factors for:

1. “Rails” to TPC OFC epoxy joints
2. TPC support arms and end-structures
3. OFC itself

new ANSYS simulations by Derek Shuman for a 10,000 lb TOF

2. assume 4-point support and 2-point support (one arm misaligned).
3. assume specific model for skin composition (glued-on rails stiffen the structure).



results for 1.

tof rails can support

3.2 klb peel

1.6 Mlb shear

2.2 Mlb tension

→ 1 klb trays would not defeat the epoxy

results for 2.

4-support max stress ~ 12.6 MPa

2-support max stress ~ 24.9 MPa

“well under yield point 214 MPa
for the H5052-H34 Al used...”

results for 3.

Tangential direction normal stresses

“are only 6.5 MPa localized near
the support in the 2-arm configuration”

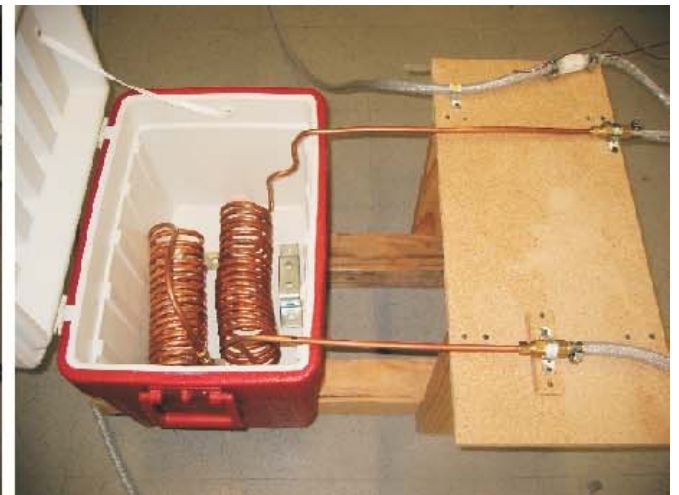
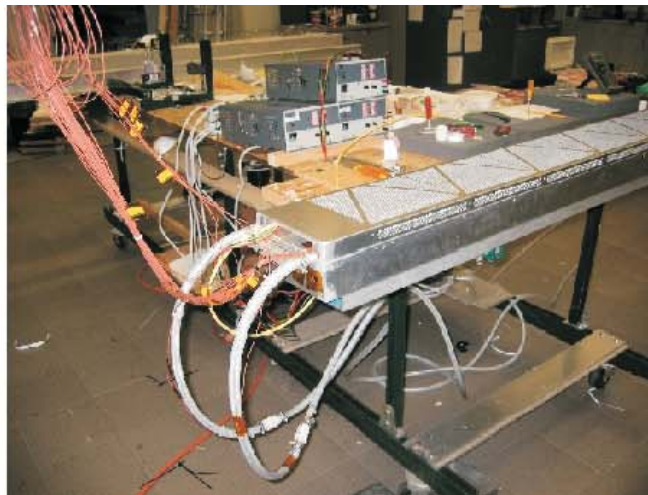
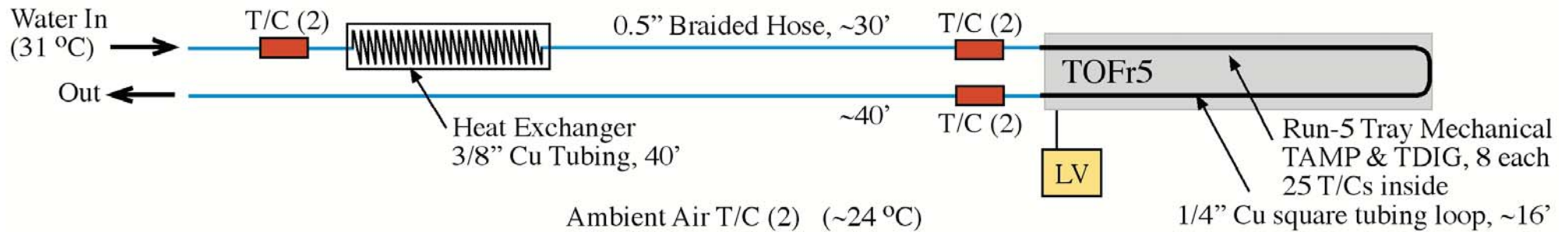
Power, Cooling, & Temperature Issues

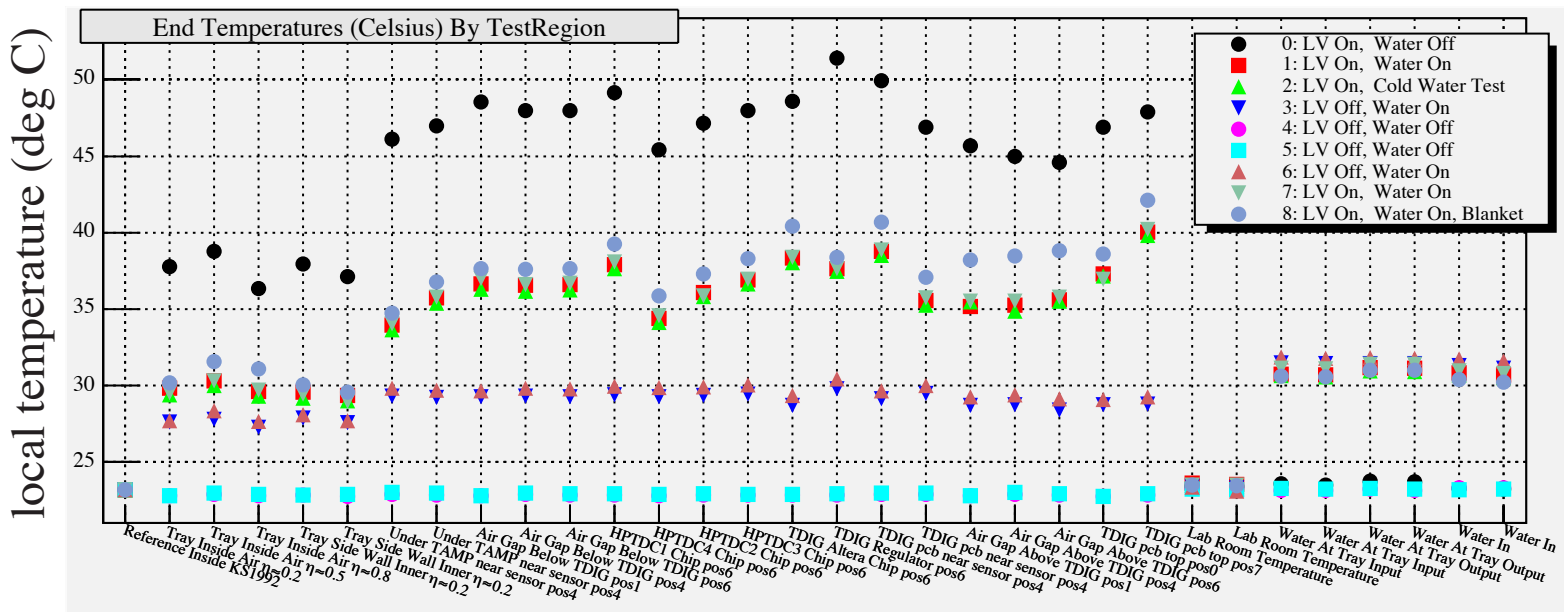
TOFr5 electronics drop 140 +/- 10 W (TOFr6 < 100W?)

Efficiency of TOFr5's embedded 1/4"-square Cu cooling loop measured at RICE
32 Type-T thermocouples inside tray, on electronics, plus ambient, water in&out, etc.
Kinetics 1992/3516 T/C readout via CAMAC to PC

measurement error <0.2 deg C

full complement of TAMP & TDIG electronics installed and powered up
water flow unfortunately 31 deg C (is <25 deg C in STAR)
perforated top assembly!

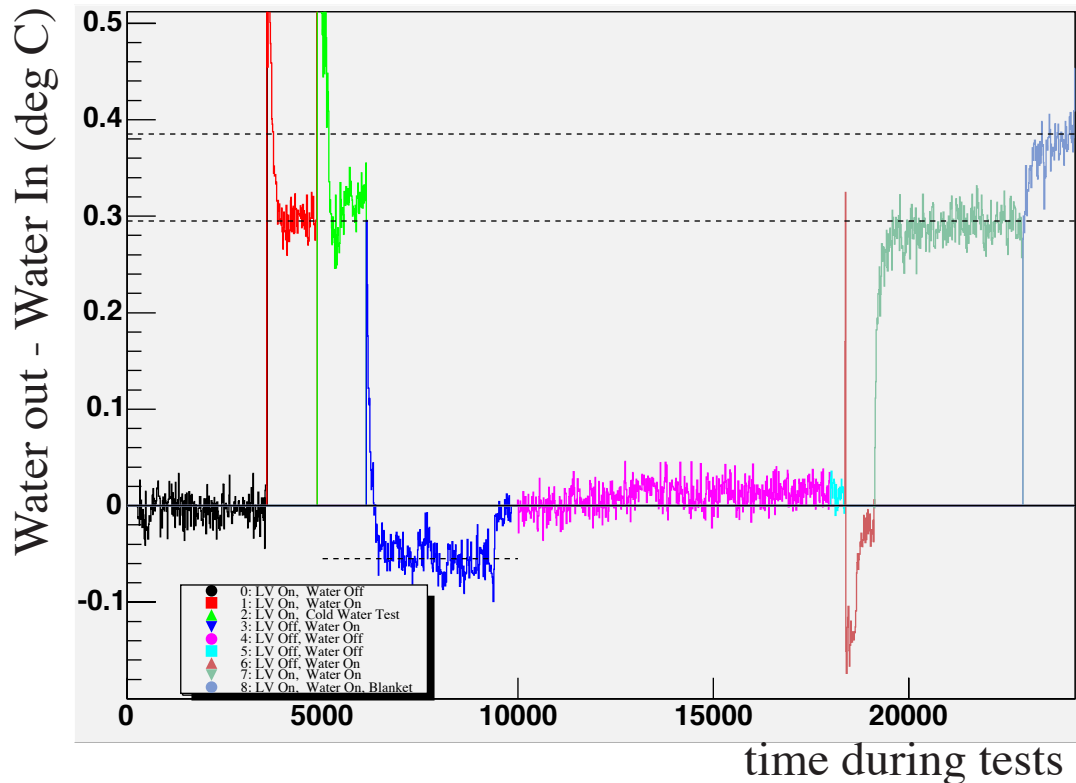




max T, water flow off
~52 deg C

HPTDC spec
<60 deg C
regulators spec
<80 deg C

max T w/ warm water
~40 deg C



Power estimates

105 W removed by (warm) water!
(~3/4 of 140W total dropped)

remainder is estimated to be:

- convective ~0W
- radiative (skin) ~3W
- radiative (FEE) ~30W

these calculations suggest radiative power could be ~halved with a solid cover...

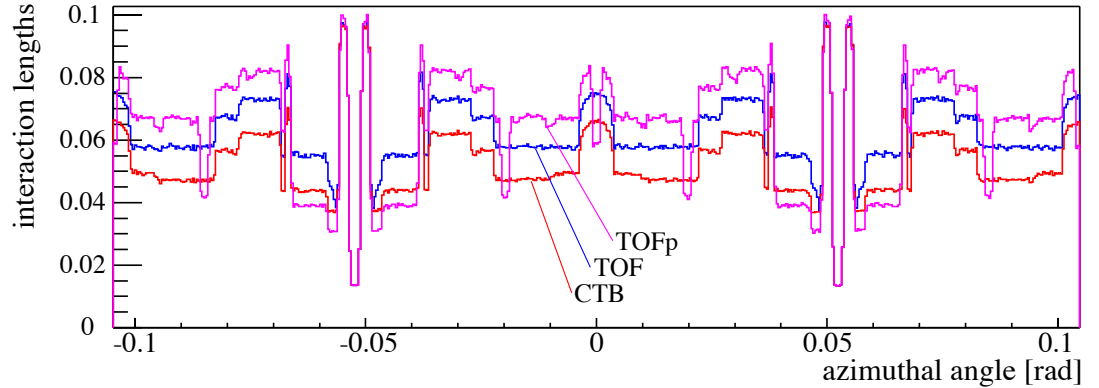
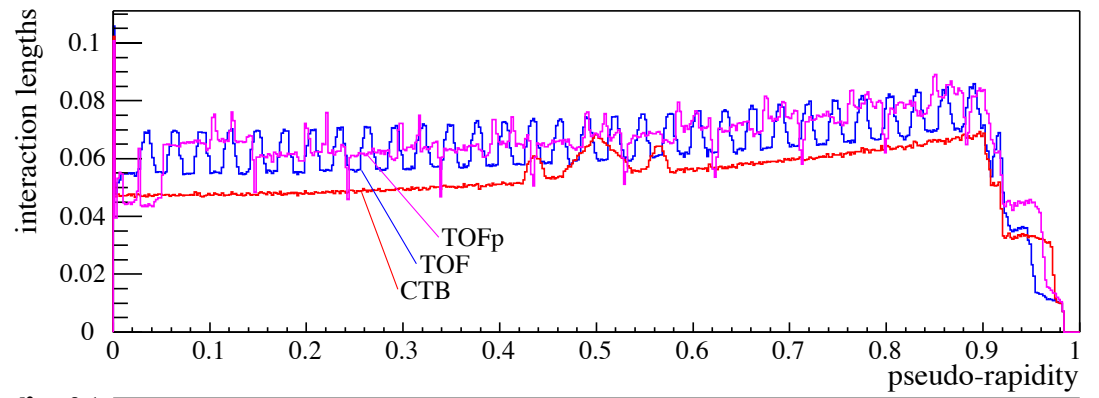
TINO also drops total power to <100 W

will repeat these tests using TOFr6 trays
both solid and perforated cover assys
both square and rectangular loops
(improved thermal efficiency)

Secondary production
estimates from AGI+gstar simulations
full description of MRPCs

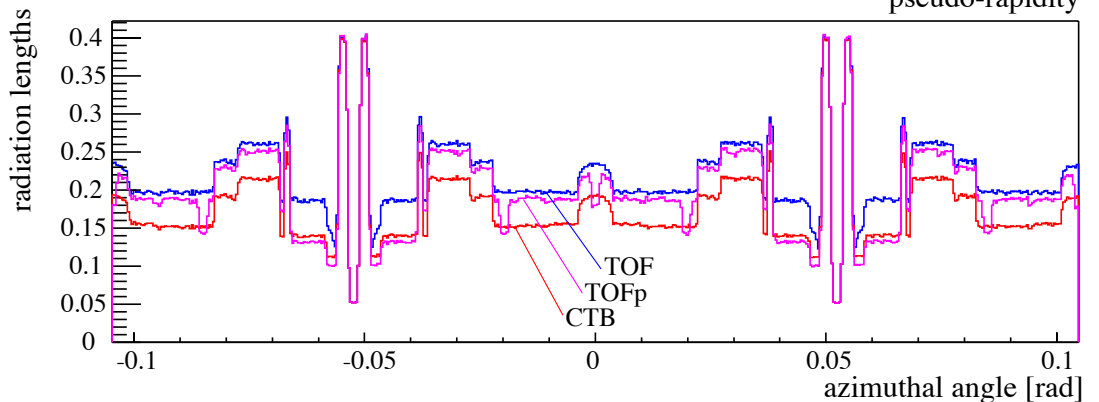
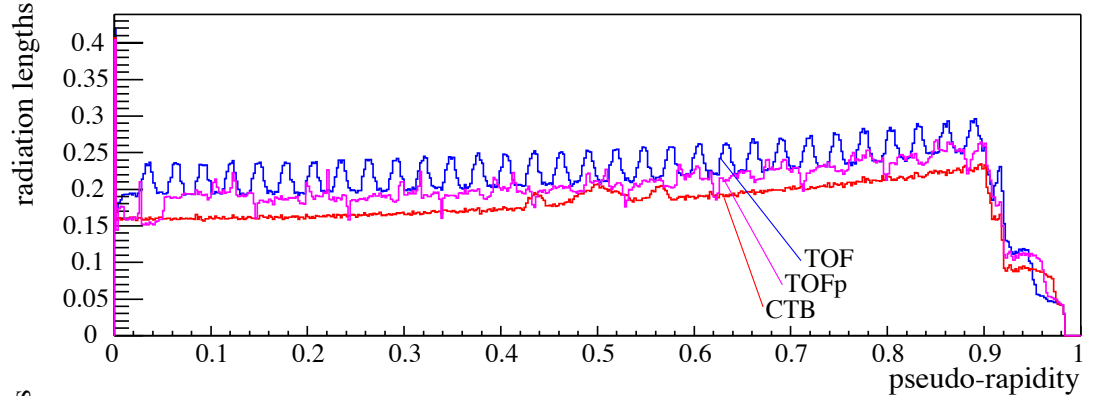
TOF: $\sim 6.5\%$ of λ_0
CTB: $\sim 4.9\%$

$\rightarrow 32\%$ more than CTB



TOF: $\sim 20\%$ of X_0
CTB: $\sim 15\%$

$\rightarrow 33\%$ more than CTB



Gas Containment

best MRPC performance obtained with 90% Freon, 5% iso-butane, & 5% SF6
most early papers on MRPC just call this “the standard mixture”

concern is the detrimental effects that SF6 would have on the TPC performance

Alice result:

http://rjd.home.cern.ch/rjd/Alice/frac_SF6.html

“...if an electron is to have a 50 % probability to survive 2.5 m drift,
the SF6 level should not exceed 2 ppb.”

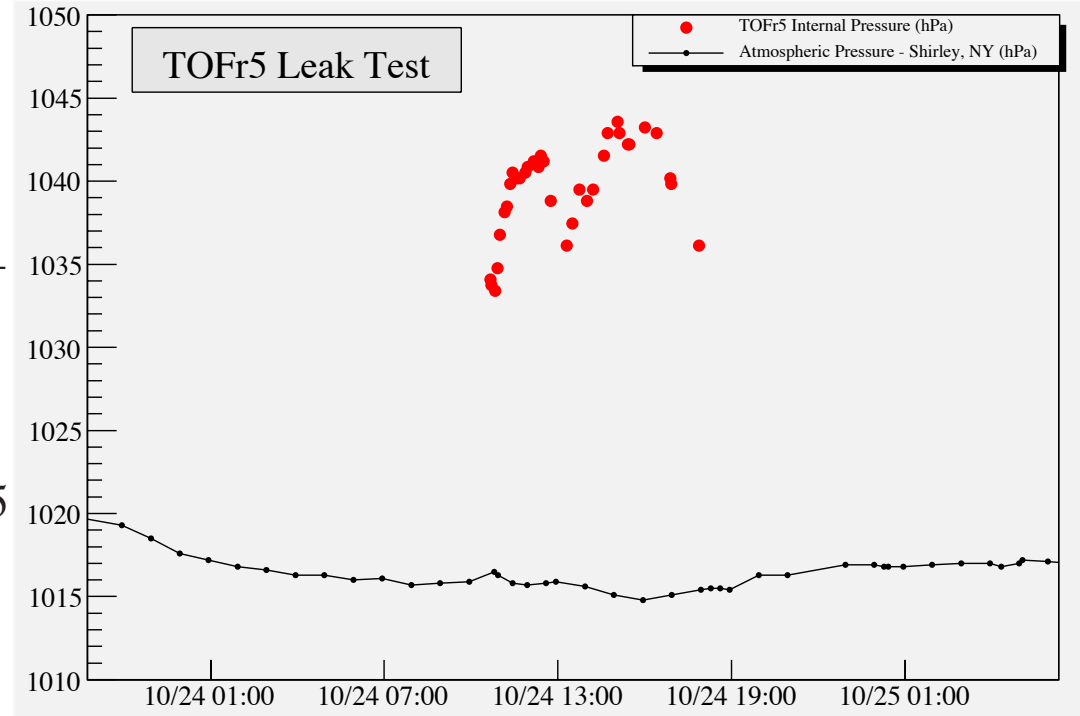
Thus, we have used only 95% Freon & 5% iso-butane during Runs 3 through 5...

measured leak rates for 3 TOFr prototypes so far

tray pressurized to ~1” above atmospheric
pressure vs time measured w/ sensitive gauge
HV connectors need to be terminated!
FEE should be **off and cool** or **on and hot!**

→ finite leak rate measured for TOFr (Run-3) -
modified CTB box
welded rail assy
glued gaskets

→ no measurable leaking for TOFr’ and TOFr5
TOFr-specific “shoe-box” style gas box
FEE sealed directly to tray aluminum



Tray Fabrication Assumptions:

- tray structures produced in Houston at Oaks Precision
QA/QC of fit & finish and size tolerances at RICE
- electronics produced in Houston (RICE, Blue Sky)
TINO on tray fabrication critical path, and must undergo stricter pre-install testing
- tray Assembly and testing at UT-Austin
MRPCs shipped to UT at rate of 160/month
bench tests of each MRPC in china and documented on WWW
no gas-box tests of MRPCs at UT before insertion into trays (except first few hundred)
size tolerance testing only
- tray retesting (HV current draw & noise rates) at BNL

Final tray fabrication follows TOFr5 model...

requires special table that can hold top+cover assembly flat and at a 90 deg angle

Working now within the group to set up the size and skewness specs & tolerances for MRPCs & Trays

manpower assumed is 2.5yr Mechanical Technician and 1 FTE undergraduate for 2yrs at UT

assumes also UT Postdoc (0.5 FTE) for Fabricated Tray testing

Rice Postdoc (0.5 FTE) for Electronics testing

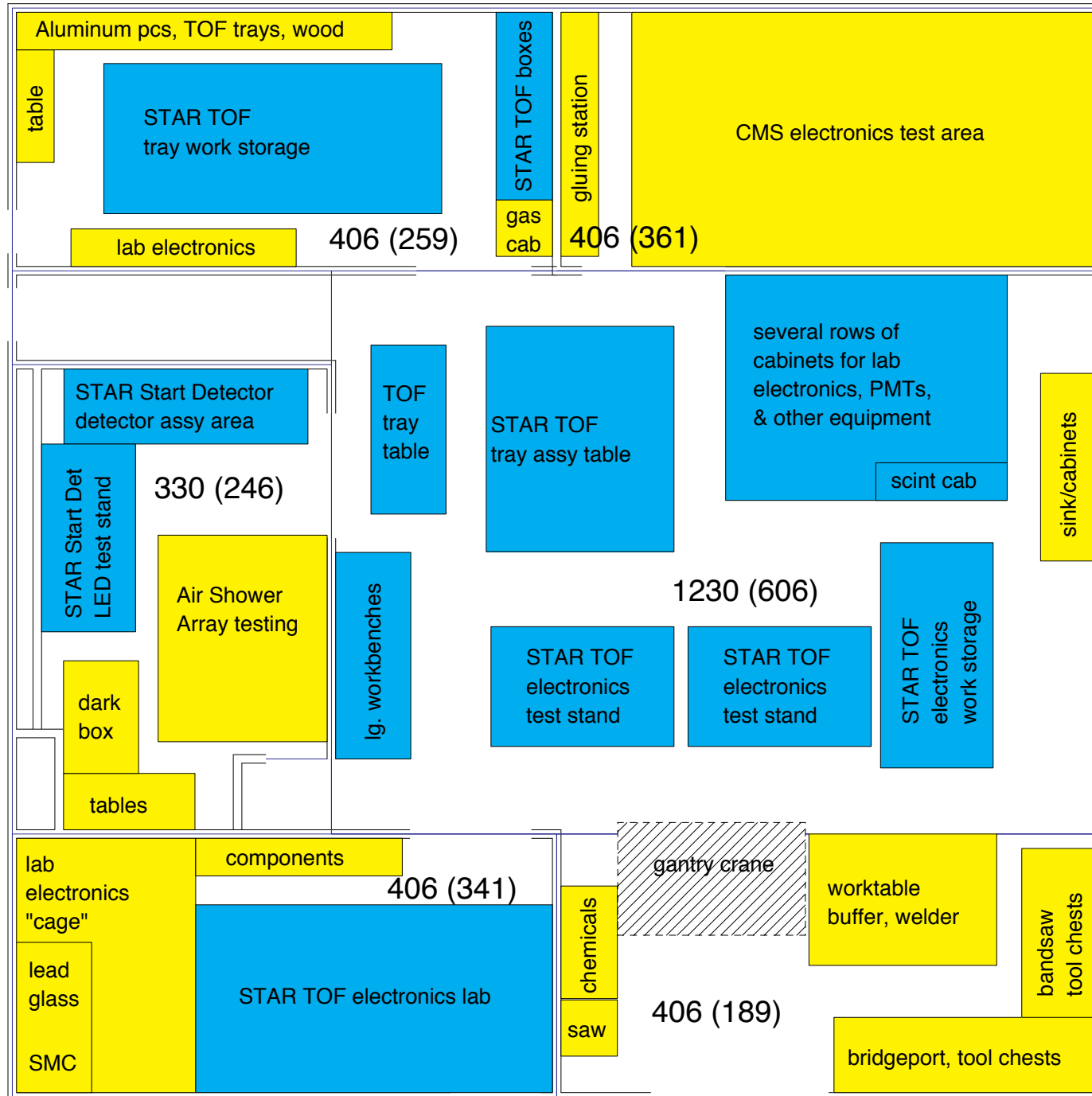
UT machine shop fabricates inner sides and cooling loops

labor is contributed...

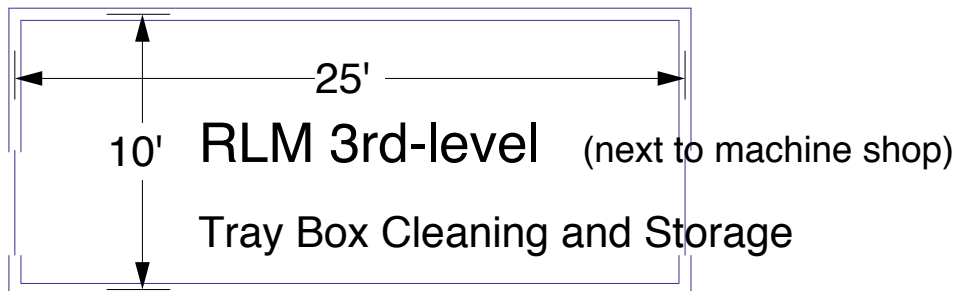
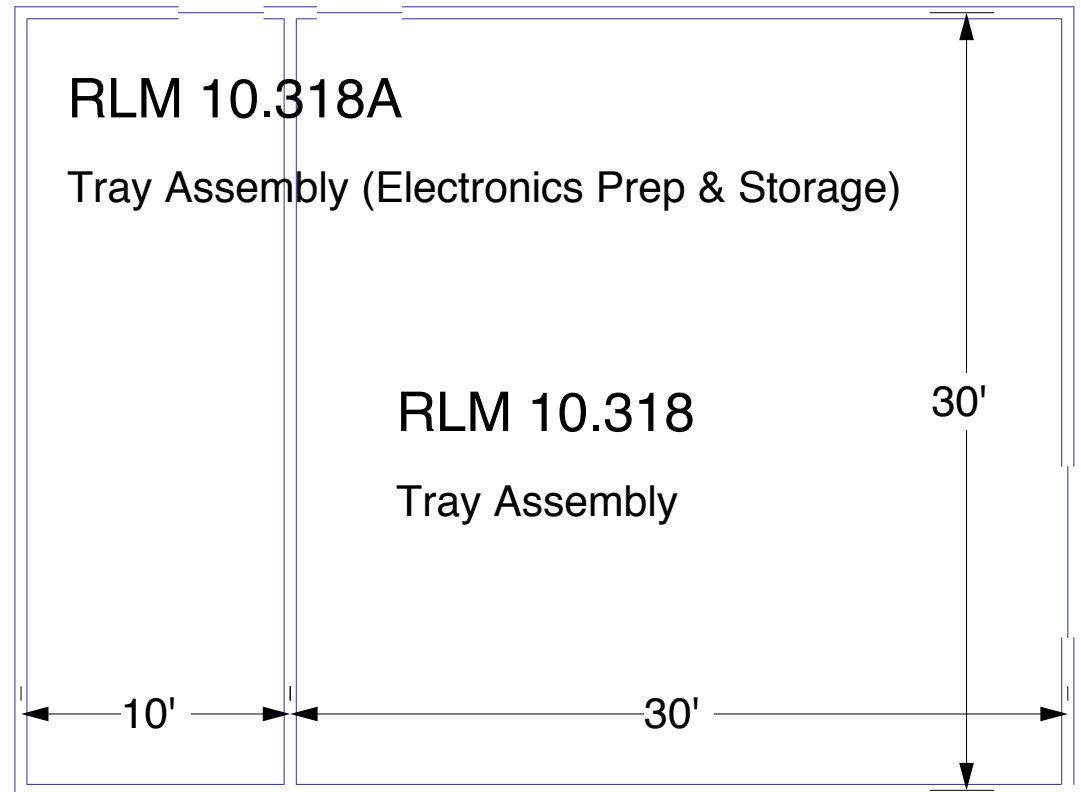
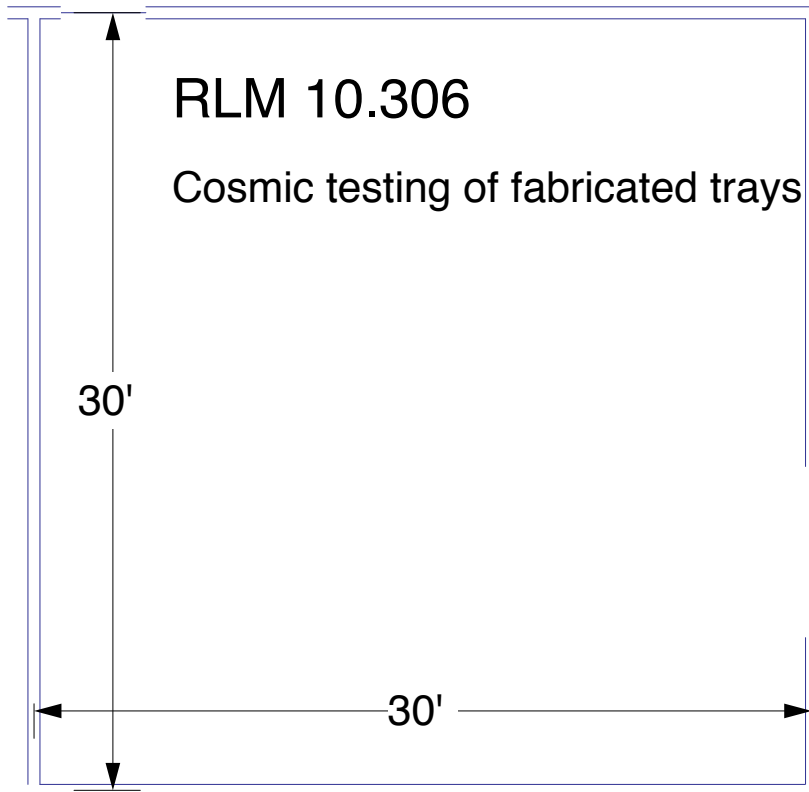
raw mtl costs only...

tray fabrication workflow and fabbed tray documentation system is under development.

Space @ RICE

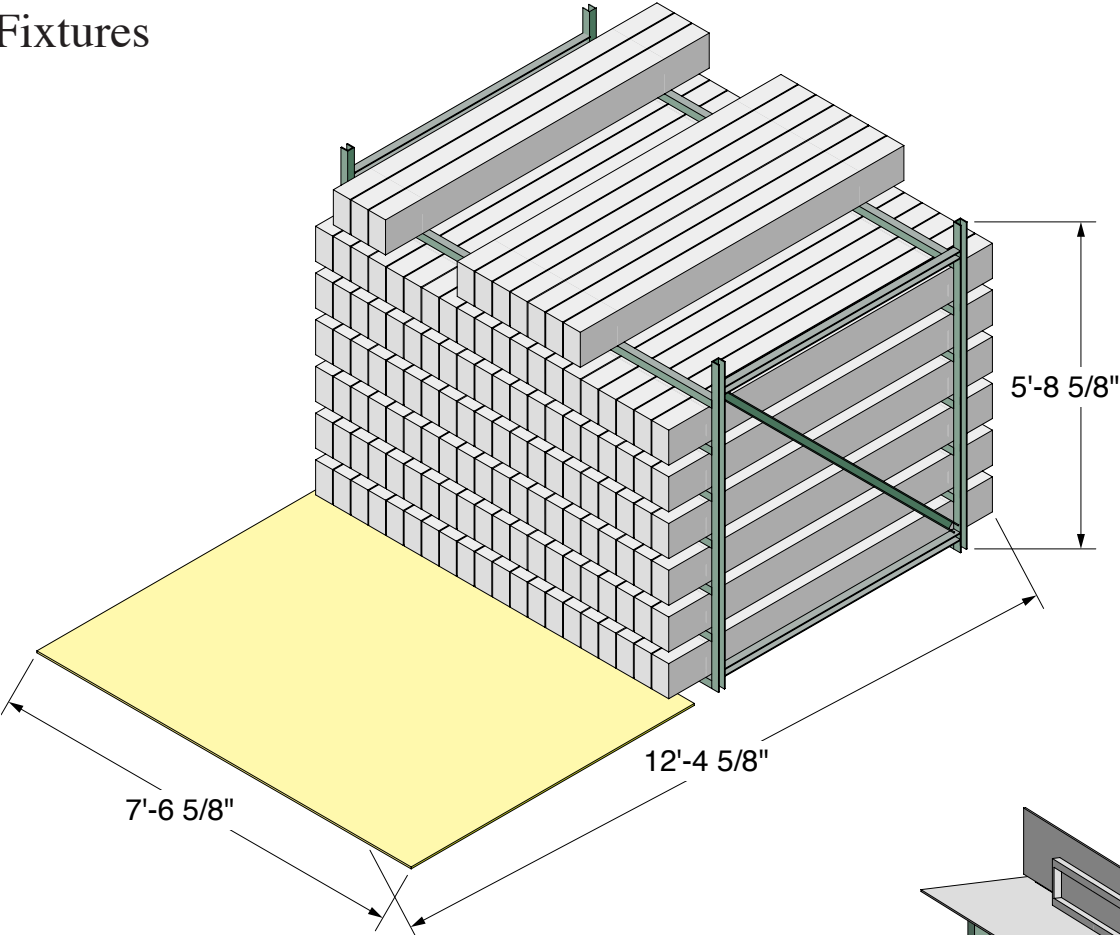


Space @ UT



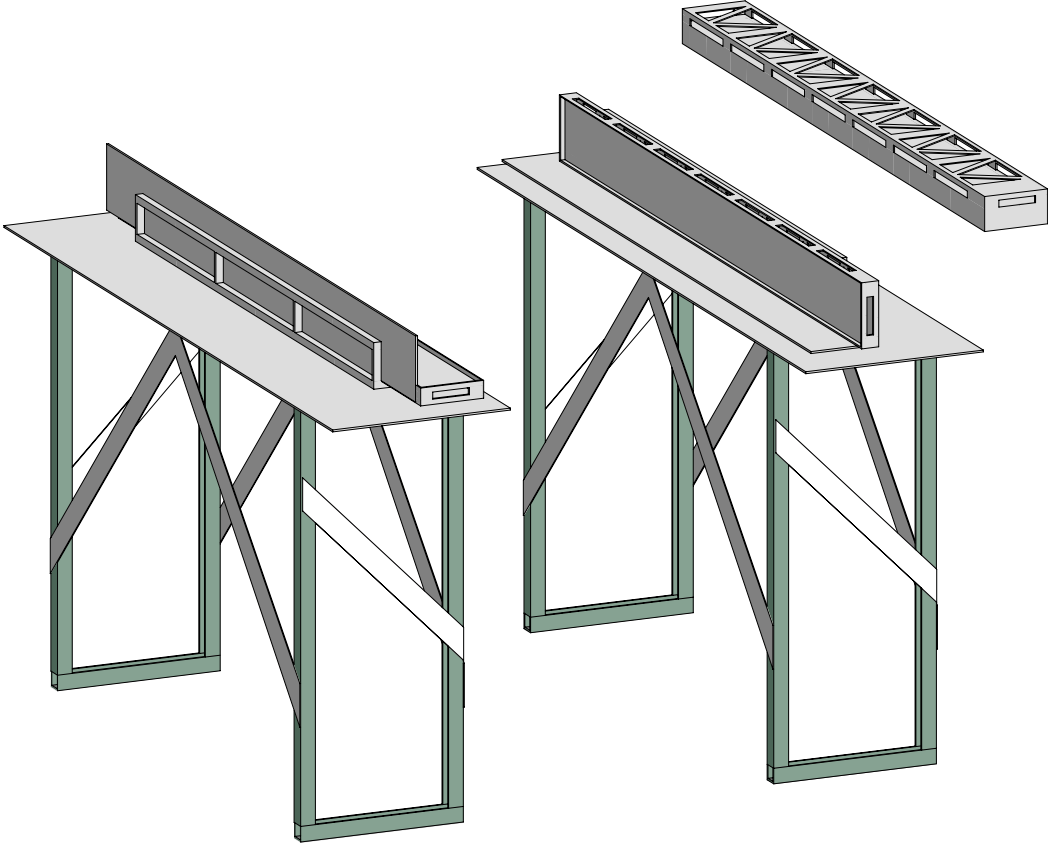
Fabricated Tray Storage and Shipping:
arbitrarily large space in
HE Physics Laboratory, ENS Bldg
(next to RLM)

Fixtures



Tray Storage Structure

Tray Assembly Fixture



general thinking is that these storage fixtures are constructed at UT during the initial 'gear-up' phase of the project i.e. during tray parts fab at Oaks...

The procedure is generally
a series of several “few minute” operations per tray
punctuated by several ~24 hrs periods of waiting per tray (sealant curing, gas flow, etc...)

Fabrication model:

at the end of each week

two trays emerge from the **tray prep area**

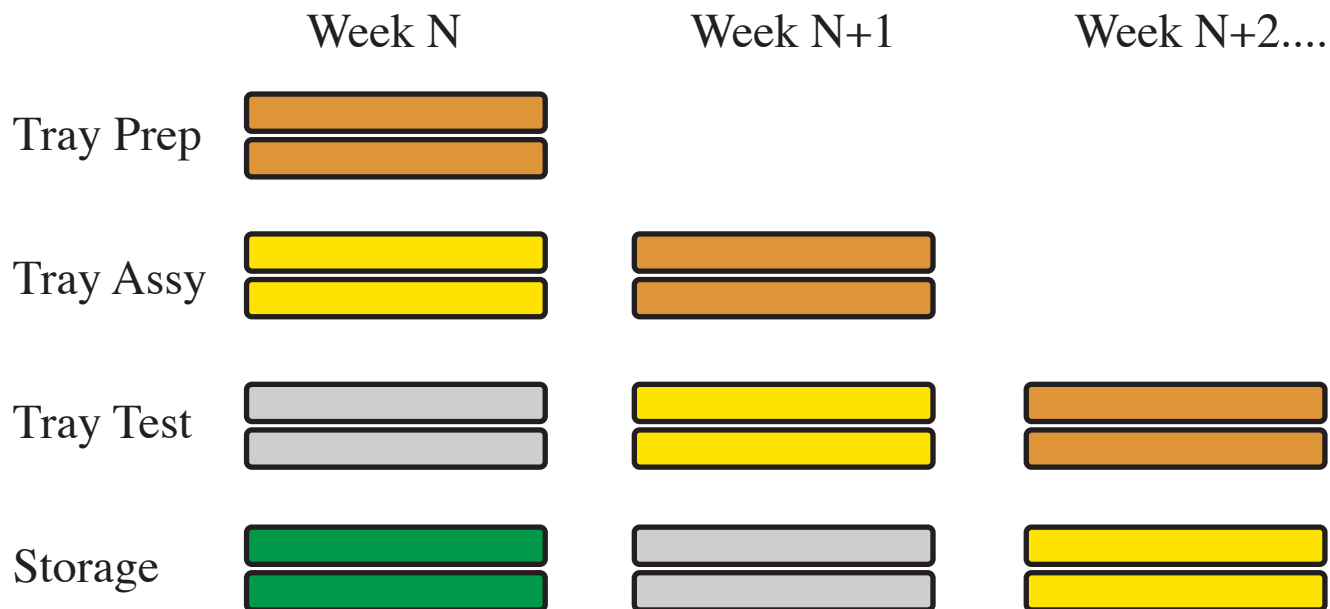
next week these will be in the **tray assembly area**

& two trays emerge from the **tray assembly area**

next week these will be in the **tray testing area** (gas flow, INL, noise rates, HV draw, etc)

Assumed manpower (1 FTE Tech + 2 FTE UG) and floor space sufficient

Gives some headroom in fabrication/testing schedule w.r.t. MRPC and FEE production



Tray Fabrication Milestones (4/year)

Date	No. Trays	No./week
10/06	4 trays	0.5 trays/week
01/07	10	0.8
04/07	10	0.8
07/07	14	1.1
10/07	14	1.1
01/08	16	1.3
04/08	18	1.5
07/08	20	1.7
09/08	20	1.7

installation plan:

“Skill-of-the-Craft”

can install either in AB or WAH

Both US & Chinese institutions participate in installation and commissioning

installation of trays behind the TPC support arms (3 & 9 o'clock, East & West)
requires a fixture to hold the TPC while one support arm is removed.

Start-Side Status and Plans

pVPD detectors still in place (4th run now) and seem to be doing as well as always...
But an increased coverage within a similar integration volume is needed

Implement prototype for Run-6, final start detector installed before FY08 with new PMTs...

Basic idea

pVPD 2" linear PMTs + significant shielding → 1.5" mesh PMTs + no shielding...
increase number of detector channels on each side within same integration volume...

same Z-location as pVPD (Runs-2 to -5) but smaller radial extent...
total weight practically unchanged

Electronics for Run-6 prototype presumably exactly the same boards as on pVPD in Run-5

HV for prototype and final system from BBC's LeCroy 1440 supply

PMTs for prototype detector will be R5946 PMTs from decommissioned TOFp
already separated from the TOFp slats, and gain & dark current tested.
Pb converter + Scint (a few chs on each side will use quartz or lead glass instead)

New PMTs for the final detector are costed
purchase FY07, to be installed in final structures and ready for FY08 run...

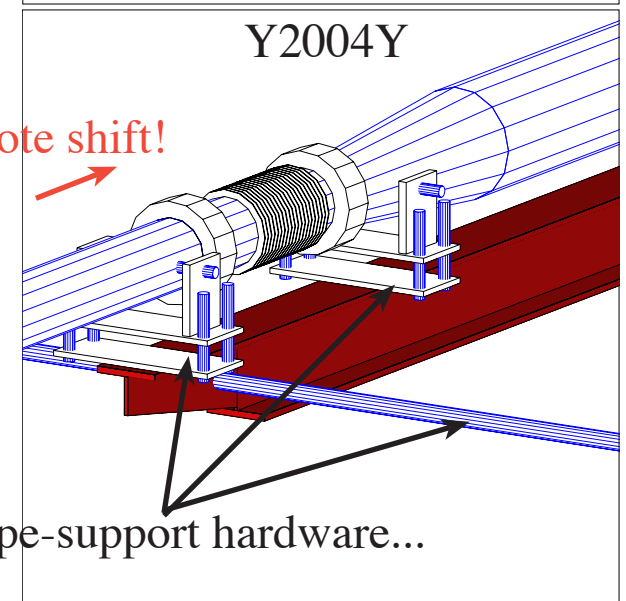
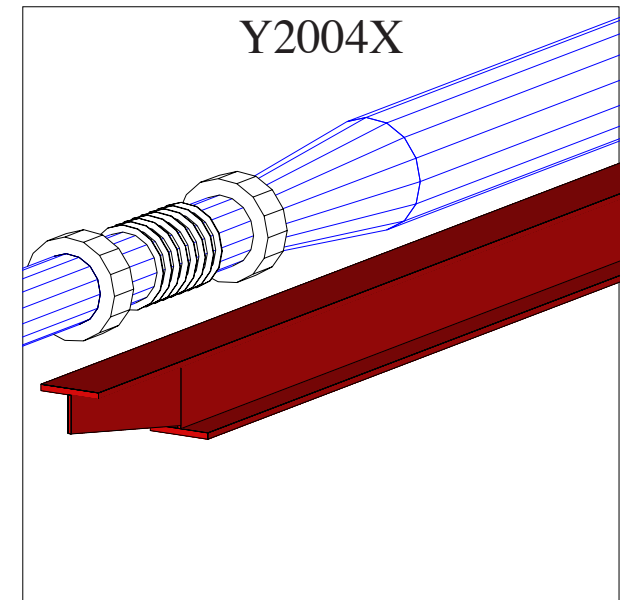
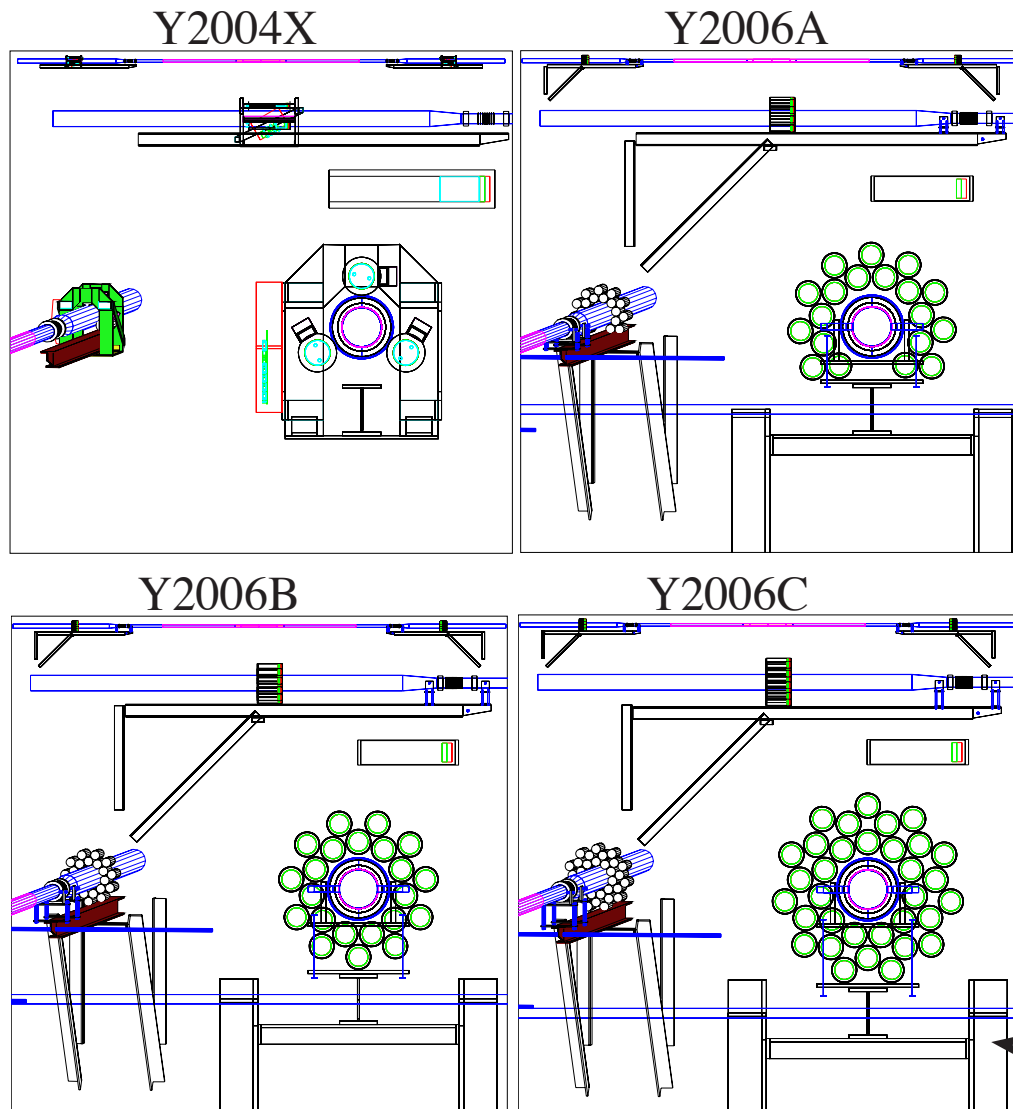
Main R&D developments:

[Detector design](#), based on full simulations

[PMT base design](#), need high stability and high rate capability

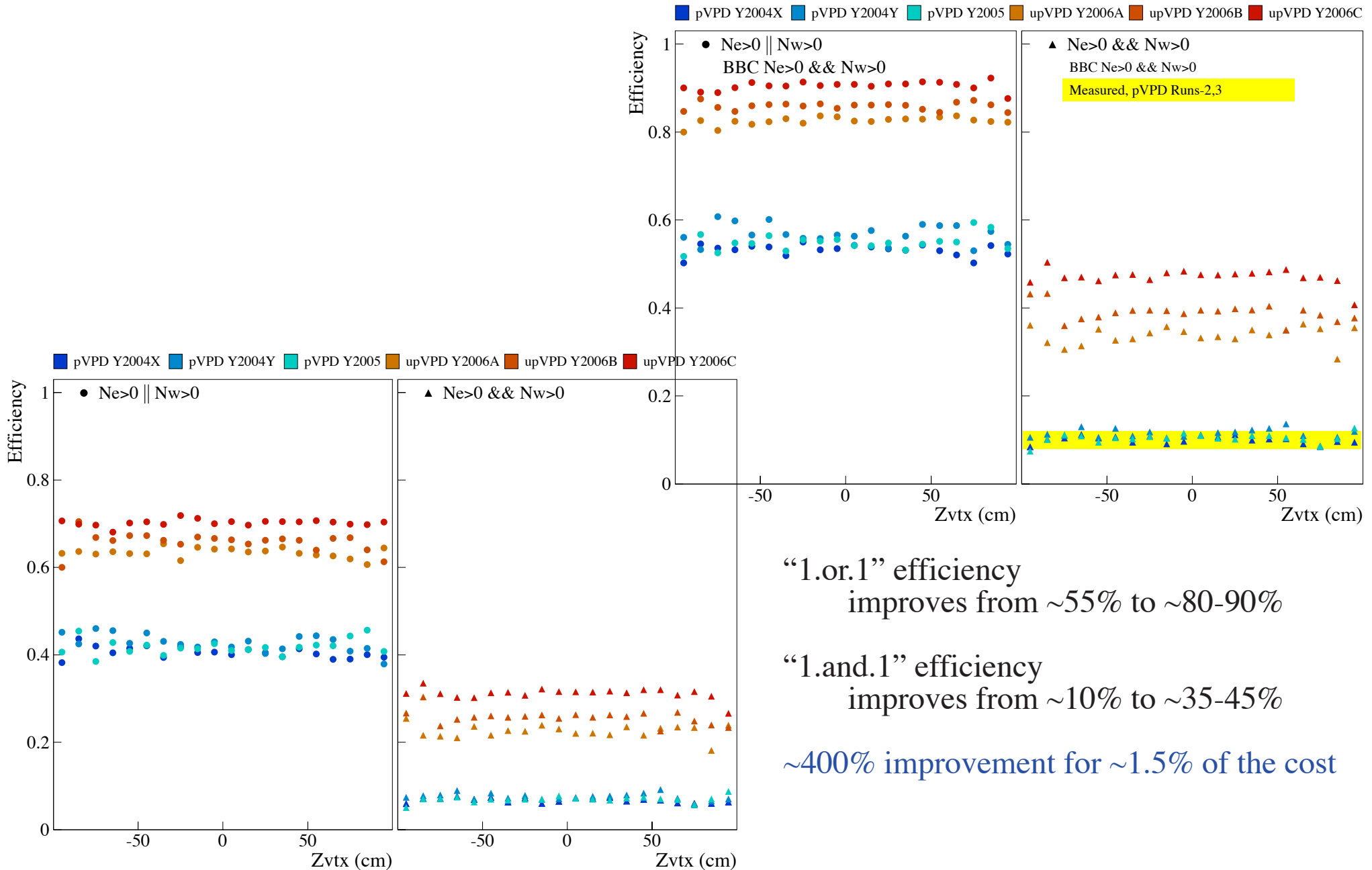
Simulations of the Upgraded pVPD (Geometry)

- Strict comparison btw starsim geometry and CADD files from STSG (discrepancies found!)
- First definition of many pipe & I-beam support structure pieces missing from starsim geometry
- Definition of several possible geometries for upVPD
- Performance of the different designs in p+p and Au+Au evts



Simulations of the Upgraded pVPD (Performance)

- concentrate on **minimum bias p+p collisions** (pythia, MSEL=2)
- study efficiency by which detector can produce start times for the different detector geometries



“1.or.1” efficiency
improves from ~55% to ~80-90%

“1.and.1” efficiency
improves from ~10% to ~35-45%

~400% improvement for ~1.5% of the cost

New Bases for the Upgraded pVPD

(Vahe Ghazikhanian, J. Mitchell, WJL)

Intended for low-power & high-rate operation with R5946 mesh PMTs

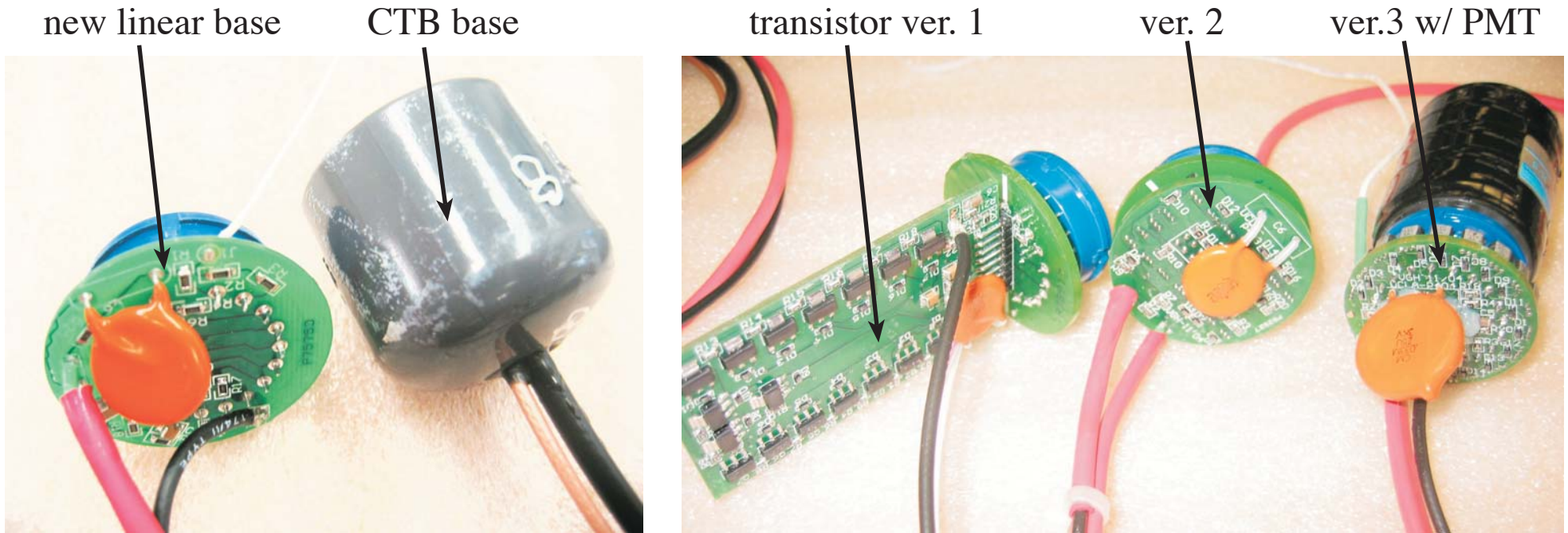
Developed one Linear base, but higher rate than std. Hamamatsu design

Linear base drops $\sim 2\text{W}$ at 2kV $\rightarrow >50\text{ }^\circ\text{C}$ inside detector assembly...

Developed 3 versions of transistor bases

MOSFETs are primary voltage divider, current $1/10^{\text{th}}$ of that for the linear base...

additional factor 10 current drop possible with different bias supply to MOSFETs (resistor chge)...



Burned-in for ~ 1 wk at UCLA, then LED rate-tested at Rice

Can't see any rate-dependent sag in any of the new bases (several nC pulses, 10's of kHz)

Parts available for ~ 3 more of latest design transistor base, will build more before Run-6

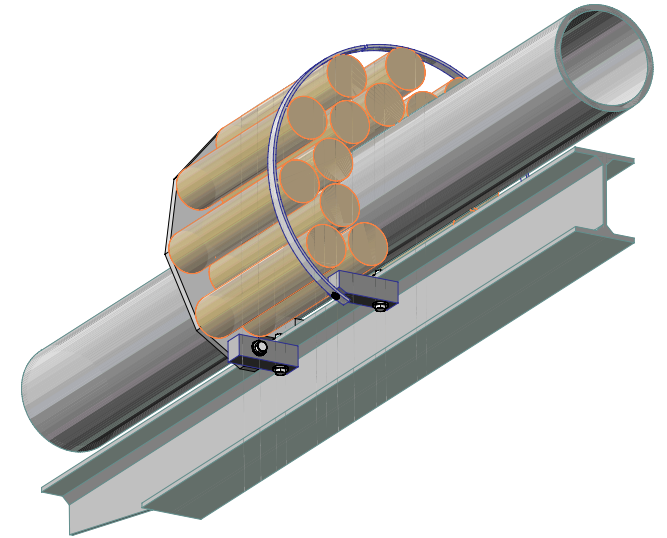
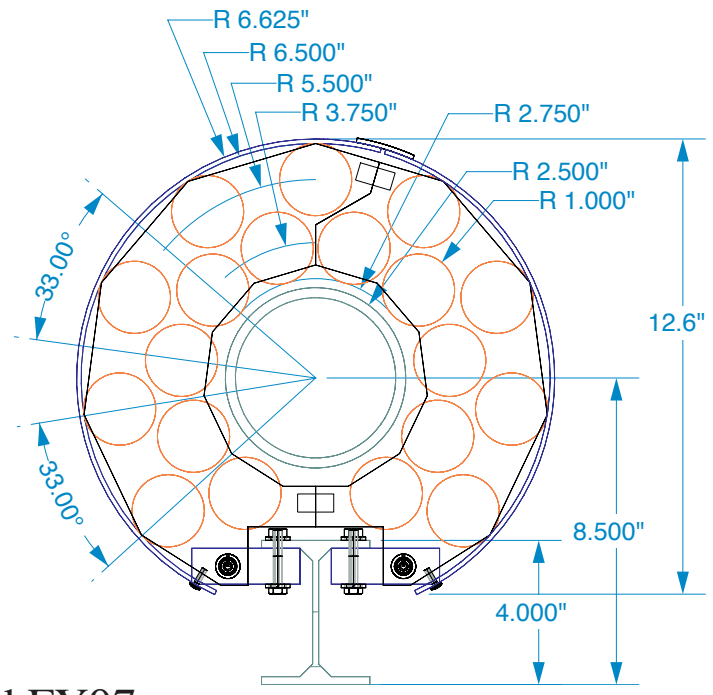
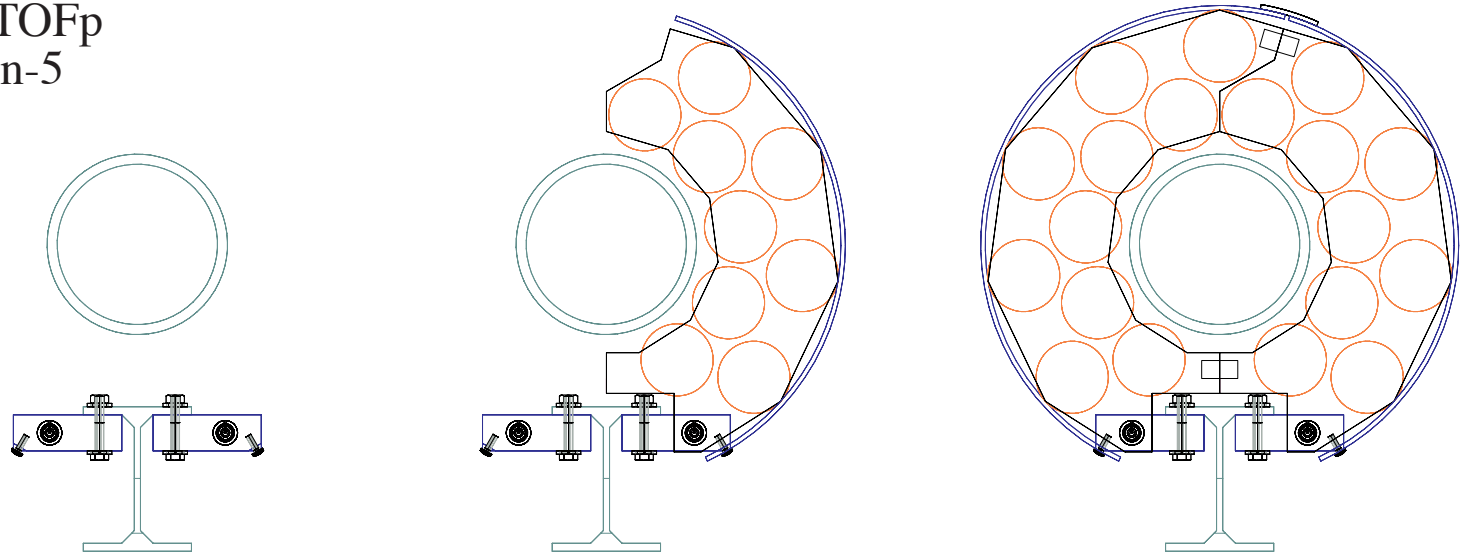
Run-6 prototype

19 detectors/side

test scintillator, quartz, and lead-glass as optical element

R5946 PMTs from TOFp

electronics from Run-5



Run-8++ "final" detector

24 chs/side

new PMTs purchased FY07